

International Journal of Statistics and Applied Mathematics

ISSN: 2456-1452
 Maths 2018; 3(1): 54-59
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 www.mathsjournal.com
 Received: 09-11-2017
 Accepted: 10-12-2017

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A study on analytical solution for acoustic waves propagation in fluids

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Abstract

In this paper, The approach is based on a analytical solution to the homogeneous wave equation for fluid medium. Analytical solution found for the acoustic waves propagation in fluid medium using normal mode analysis and discuss the computational results.

Keywords: Analytical solution, acoustic waves, propagation in fluids

1. Introduction

In recent years, physical acoustic wave modeling has become a successful tool in diagnostic and therapeutic ultrasound application. There are several wave equations available for describing acoustic wave propagation. Numerical methods can be used as a tool for sound field simulation. Discrete-time simulation algorithms for wave propagation can be derived by numerically solving an acoustic wave equation in terms of the variables for sound pressure and particle velocity. Initial conditions for time derivatives and boundary conditions for space derivatives are necessary to provide a complete set of solutions of the wave equation. These equations are most commonly solved by propagation in time. However, when propagating over large distances, such methods are expensive in terms of memory and computational costs. The normal mode analysis method gives exact solutions without any assumed restrictions on pressure and velocity components distributions. It is applied to wide range of problems in different branches. It can be applied to boundary-layer problems, which are described by the linearized Navier-stokes equations in electrohydrodynamic.

In this paper, the normal mode analysis can be employed to solve linear acoustic wave equation analytically. The technique focuses on description of a linear model and discusses the conditions under which using this technique. The propagation of acoustic pressure wave by the normal mode analysis in a medium with two-dimensional spatially variable acoustic properties has been explained.

2. Acoustic Wave Equation

Consider sound waves propagating in the water. Instead of the wave equation, we base our work on the basic Euler's equation and the equation of continuity. For simplicity, the discussion is confined to a two dimensional space. In a 2-D Cartesian coordinate system, the sound pressure p and the particle velocity \mathbf{v} satisfy the following linear equations:

$$-\rho \nabla \cdot \mathbf{v}(x, y, t) = \frac{1}{c^2} \frac{\partial p(x, y, t)}{\partial t} \quad \dots(2.1)$$

$$\frac{\partial p(x, y, t)}{\partial x} = -\rho \frac{\partial v_x(x, y, t)}{\partial t} \quad \dots(2.2)$$

$$\frac{\partial p(x, y, t)}{\partial y} = -\rho \frac{\partial v_y(x, y, t)}{\partial t} \quad \dots(2.3)$$

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where $v(x, y, t) = \hat{x}v_x(x, y, t) + \hat{y}v_y(x, y, t)$ is the particle velocity, $p(x, y, t)$ is the pressure and ρ is the density of the fluid with wave number $k = \frac{\omega}{c} + i\alpha$ where $i = \sqrt{-1}$, ω is angular frequency, c and α are the speed of sound and attenuation in homogenous medium, respectively.

Normal Mode Analysis

The solution of considered physical variable can be decomposed in terms of normal modes as the following form

$$[v_x, v_y, p](x, y, t) = [v_x^*, v_y^*, p^*](x)e^{i(\omega t + ky)} \dots(2.4)$$

Where v_x^*, v_y^* and p^* are the amplitude of the functions v_x, v_y and p respectively.

Equation (2.1) becomes

$$\begin{aligned}
 -\rho \nabla \cdot v(x, y, t) &= \frac{1}{c^2} \frac{\partial p(x, y, t)}{\partial t} \\
 -\rho \left(\hat{x} \frac{\partial}{\partial x} + \hat{y} \frac{\partial}{\partial y} \right) (\hat{x}v_x(x, y, t) + \hat{y}v_y(x, y, t)) &= \frac{1}{c^2} \frac{\partial p(x, y, t)}{\partial t} \\
 -\rho \left(\frac{\partial v_x(x, y, t)}{\partial x} + \frac{\partial v_y(x, y, t)}{\partial y} \right) &= \frac{1}{c^2} \frac{\partial p(x, y, t)}{\partial t}
 \end{aligned}$$

Apply equation (2.4) in above equation

$$\begin{aligned}
 -\rho \left(\frac{\partial v_x^*(x)e^{i(\omega t + ky)}}{\partial x} + \frac{\partial v_y^*(x)e^{i(\omega t + ky)}}{\partial y} \right) &= \frac{1}{c^2} \frac{\partial p^*(x)e^{i(\omega t + ky)}}{\partial t} \\
 -\rho (Dv_x^*(x)e^{i(\omega t + ky)} + v_y^*(x)e^{i(\omega t + ky)} \cdot ik) &= \frac{1}{c^2} p^*(x)e^{i(\omega t + ky)} \cdot i\omega \\
 e^{i(\omega t + ky)} (-\rho Dv_x^* - i\rho kv_y^*) &= \frac{i\omega}{c^2} p^*(x)e^{i(\omega t + ky)} \\
 -\rho Dv_x^* - i\rho kv_y^* &= \frac{i\omega}{c^2} p^* \dots(2.5)
 \end{aligned}$$

Applying (2.4) in Equation (2.2)

$$\begin{aligned}
 \frac{\partial p^*(x)e^{i(\omega t + ky)}}{\partial x} &= -\rho \frac{\partial v_x^*(x)e^{i(\omega t + ky)}}{\partial t} \\
 Dp^* e^{i(\omega t + ky)} &= -\rho v_x^* e^{i(\omega t + ky)} \cdot i\omega \\
 Dp^* &= -i\rho\omega v_x^* \dots(2.6)
 \end{aligned}$$

Applying (2.4) in equation (2.3)

$$\begin{aligned}
 \frac{\partial p^*(x)e^{i(\omega t + ky)}}{\partial y} &= -\rho \frac{\partial v_y^*(x)e^{i(\omega t + ky)}}{\partial t} \\
 p^* e^{i(\omega t + ky)} \cdot ik &= -\rho v_y^* e^{i(\omega t + ky)} \cdot i\omega \\
 kp^* &= -\rho\omega v_y^* \dots(2.7)
 \end{aligned}$$

Where $D = \frac{\partial}{\partial x}$

Equation (2.5) – (2.7) form a coupled system.

Eliminating v_x^* and v_y^* values in equation (2.5)

$$v_x^* = -\frac{1}{i\rho\omega} Dp^* \quad \dots(2.8)$$

$$v_y^* = -\frac{k}{\rho\omega} p^* \quad \dots(2.9)$$

Substitute v_x^* and v_y^* values in equation (2.5)

$$\begin{aligned} -\rho D\left(-\frac{1}{i\rho\omega} Dp^*\right) - i\rho k\left(-\frac{k}{\rho\omega} p^*\right) &= \frac{i\omega}{c^2} p^* \\ -iD^2 p^* + ik^2 p^* &= \frac{i\omega^2}{c^2} p^* \\ D^2 p^* - k^2 p^* + \frac{\omega^2}{c^2} p^* &= 0 \\ D^2 p^* - \left(k^2 - \frac{\omega^2}{c^2}\right) p^* &= 0 \\ D^2 p^* - m^2 p^* &= 0 \end{aligned} \quad \dots(2.10)$$

Where, $m^2 = \left(k^2 - \frac{\omega^2}{c^2}\right)$

The solution of equation (2.10) has the form

$$p^*(x) = \sum_{i=1}^2 p_i^* \quad \dots(2.11)$$

Where $p_i^* = G_i(k, \omega)e^{r_i x}$, and r_i are the roots of the characteristic equation.

$$\begin{aligned} r_i^2 - m^2 &= 0 \\ r_i &= \pm m \end{aligned} \quad \dots(2.12)$$

The solution of equation (2.10) is given by

$$p^*(x) = G_1(k, \omega)e^{-mx} + G_2(k, \omega)e^{mx} \quad \dots(2.13)$$

Substitute p^* values in equation (2.8)

$$\begin{aligned} v_x^* &= -\frac{1}{i\rho\omega} D(G_1(k, \omega)e^{-mx} + G_2(k, \omega)e^{mx}) \\ &= -\frac{1}{i\rho\omega} (-mG_1(k, \omega)e^{-mx} + mG_2(k, \omega)e^{mx}) \\ v_x^* &= \frac{m}{i\rho\omega} G_1(k, \omega)e^{-mx} - \frac{m}{i\rho\omega} G_2(k, \omega)e^{mx} \end{aligned} \quad \dots(2.14)$$

$$v_x^* = G_1'(k, \omega)e^{-mx} + G_2'(k, \omega)e^{mx} \quad \dots(2.15)$$

Where $G_1'(k, \omega) = \frac{m}{i\rho\omega} G_1(k, \omega)$, $G_2'(k, \omega) = -\frac{m}{i\rho\omega} G_2(k, \omega)$... (2.16)

Substitute p^* values in equation (2.9)

$$v_y^* = -\frac{k}{\rho\omega} (G_1(k, \omega)e^{-mx} + G_2(k, \omega)e^{mx})$$

$$v_y^* = -\frac{k}{\rho\omega} G_1(k, \omega)e^{-mx} - \frac{k}{\rho\omega} G_2(k, \omega)e^{mx} \quad \dots(2.17)$$

$$v_y^* = G_1''(k, \omega)e^{-mx} + G_2''(k, \omega)e^{mx} \quad \dots(2.18)$$

$$\text{Where } G_1''(k, \omega) = -\frac{k}{\rho\omega} G_1(k, \omega), G_2''(k, \omega) = -\frac{k}{\rho\omega} G_2(k, \omega) \quad \dots(2.19)$$

Boundary Condition

On the surface at x=0

$$v_x^* = F(y, t), p^* = p_0(y, t) \quad \dots(2.20)$$

Substituting from (2.4) into (2.20)

$$v_x^* = F_0^*, p^* = p_0^*$$

at x=0 equation (2.13) becomes

$$p_0^* = G_1 + G_2 \quad \dots(2.21)$$

Equation (2.14) becomes

$$F_0^* = \frac{m}{i\rho\omega} (G_1 - G_2)$$

$$\frac{i\rho\omega}{m} F_0^* = G_1 - G_2 \quad \dots(2.22)$$

By adding equation (2.21) and (2.22) we obtain

$$G_1 = \frac{1}{2} (p_0^* + \frac{i\rho\omega}{m} F_0^*) \quad \dots(2.23)$$

By subtracting equation (2.21) and (2.22) we obtain

$$G_2 = \frac{1}{2} (p_0^* - \frac{i\rho\omega}{m} F_0^*) \quad \dots(2.24)$$

By substituting from equation (2.23) and (2.24) into the equation

(2.13), (2.14) and (2.17)

$$p(x, y, t) = p^*(x) e^{i(\omega t + ky)}$$

$$p(x, y, t) = (G_1(k, \omega)e^{-mx} + G_2(k, \omega)e^{mx}) e^{i(\omega t + ky)} \quad \dots(2.25)$$

$$v_x(x, y, t) = v_x^* e^{i(\omega t + ky)}$$

$$v_x(x, y, t) = \frac{m}{i\rho\omega} (G_1(k, \omega)e^{-mx} - G_2(k, \omega)e^{mx}) e^{i(\omega t + ky)} \quad \dots(2.26)$$

$$v_y(x, y, t) = v_y^* e^{i(\omega t + ky)}$$

$$v_y(x, y, t) = -\frac{k}{\rho\omega} (G_1(k, \omega)e^{-mx} + G_2(k, \omega)e^{mx}) e^{i(\omega t + ky)} \quad \dots(2.27)$$

3. Computational Results

To study the wave propagation phenomenon in viscous medium and under different frequencies, we can apply the theoretical acoustic viscous wave Equation (2.25). Using water as the medium, the parameters are given as following: $\rho = 998 \text{ Kg / m}^3$ and $c = 1481 \text{ m/s}$. Let the wave peak amplitude be $p_0^* = 1 \text{ Pa}$ and $F_0^* = 1 \text{ m/s}$ at the source ($x=0$), we simulate the pressure wave peak amplitude, in Equation (2.25), the distance from the source at various frequencies. The results are shown in Figure 1 (in dB and linear scale). As expected, the peak wave amplitude becomes smaller as we move further from the source. We can also notice that as the wave frequency goes higher, more attenuation can be observed at any given location. The peak pressure as function of frequency shown in Figure 2 for fixed distance at $x = 2 \text{ cm}$. It is clear from this figure that the magnitude of peak of pressure little changes with the frequency.

Let us consider a 2-D simulation in which the pressure varies in the x and y directions. Figure 3 shows the 2-D pressure computational as function in the plane x - y . From this figure, it can be seen that the pressure amplitude becomes smaller when moving in the x - y plane further from the source.

Pressure amplitude (dB) as function of the distance from the origin

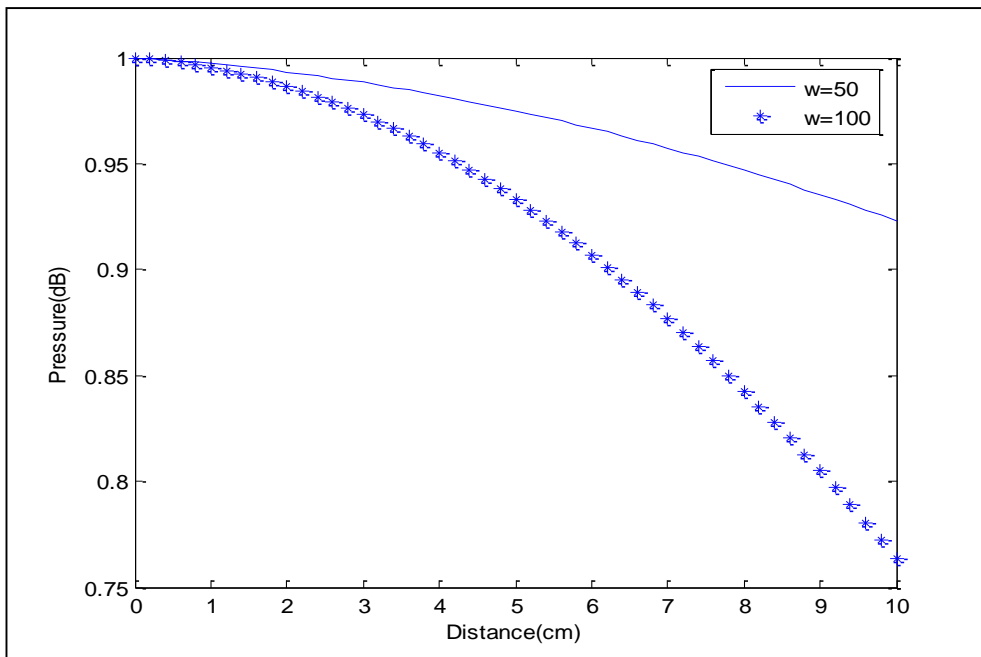


Fig 1

The pressure amplitude as function of frequency at distance 2 cm from the source

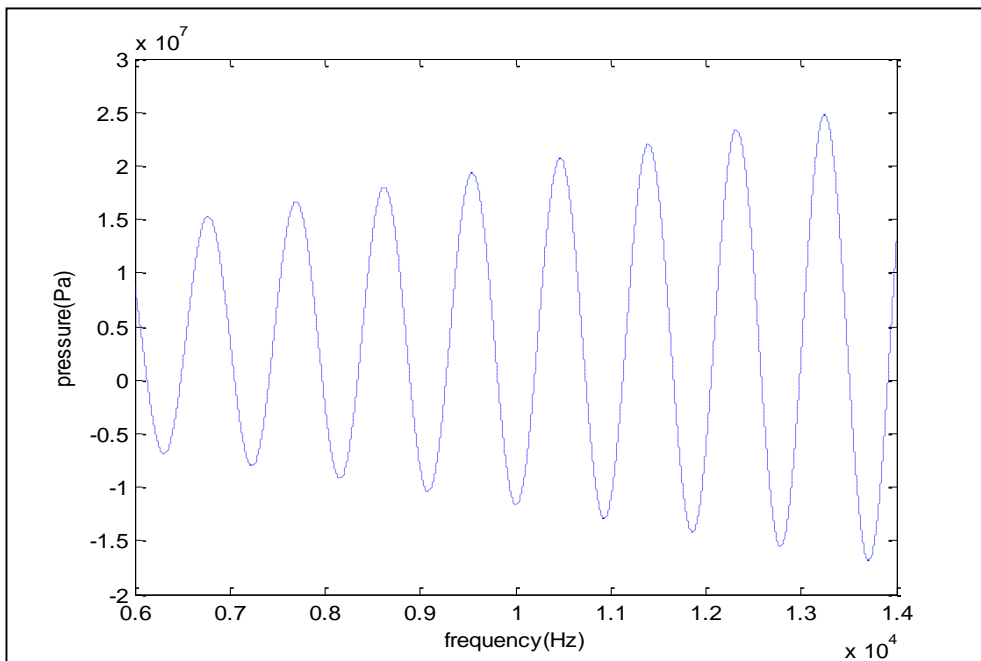


Fig 2

The pressure amplitude as function of plane x-y direction

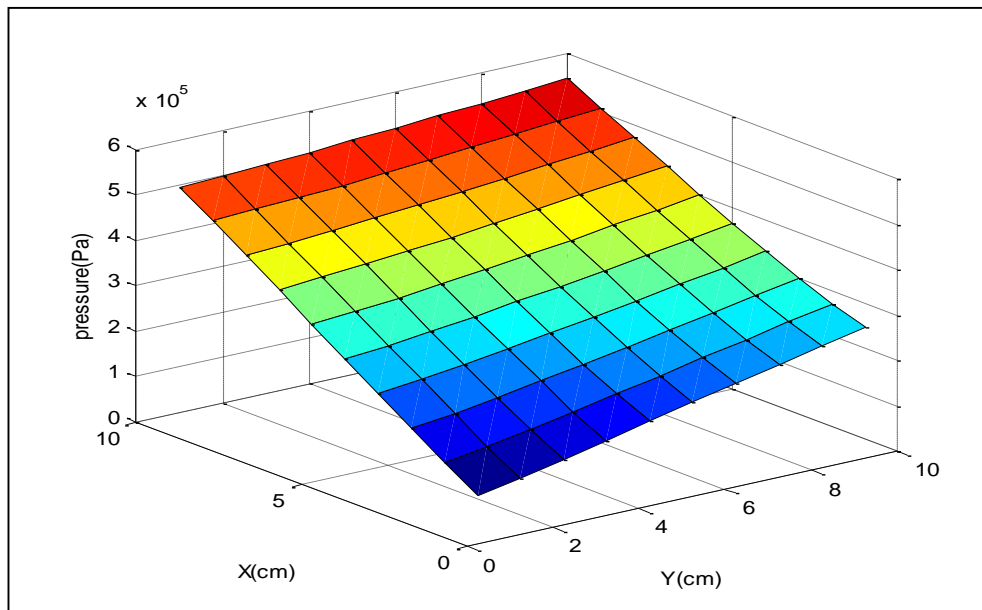


Fig 3

4. Conclusion

A normal mode analysis which accurately the pressure acoustic wave equation, has been developed. This technique has a number of attractive features, foremost of which is the speed and simplicity with which it can be designed and implemented. The model could be used in the future to incorporate non-linear propagation effects.

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